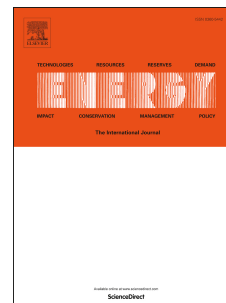


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Assessing the impact of extreme heatwaves and urban-rural climate disparities on building cooling energy demand of public rental housing in Hong Kong

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Abstract:

Urban building energy demand under heatwaves is a rising concern, which is affected by local climate conditions. This study examines how extreme heatwaves and urban–rural climate differences affect cooling energy demand in public rental housing (PRH) in Hong Kong during 2022–2024. Four typical PRH sites were selected, three on the Kowloon Peninsula and one on a built-up island, and analyzed using building energy modeling driven by locally measured urban weather data and reference rural site weather data. Weather data indicate that urban–rural air and dew point temperature differences intensify during extreme heatwave (EH) versus normal summer (NS) days. The urban-rural difference in daily accumulated total cooling load intensity (CL_{tot}) varies by urban site location, ranging from 3.8% lower to 4.0% higher in urban sites than the rural reference sites in EH days. A diurnal pattern is observed: At night (23:00 to 06:00), the accumulative total cooling load intensity is mostly higher than that from the reference rural site, reaching up to 17.4% higher in EH days and 24.3% higher in NS days. During the remainder of the day (07:00–22:00), the urban site generally results in a lower total cooling load intensity, up to 7.4% lower in EH days and 6.5% lower in NS days, than that from the reference rural site. Sensible cooling load is primarily associated with air temperature, whereas latent cooling load exhibits location-dependent responses to dew point temperature.

Keywords:

Building Energy Efficiency; Urban Microclimate; Heat Island; Urban Heat; Urban Climate; Public Rental Housing

1. Introduction

Anthropogenic climate change is intensifying numerous weather and climate extremes across the globe. According to the Intergovernmental Panel on Climate Change (IPCC), the period between 2010 and 2019 marked the highest decadal greenhouse gas (GHG) emissions ever documented. This trajectory is fundamentally altering global climate patterns, leading to an anticipated rise in the regularity of extreme weather events, including heatwaves [1]. These climatic pressures are often intensified by the morphological and thermal characteristics of the built environment, manifested by the Urban Heat Island (UHI) effect [2-4], Urban Cool Island (UCI) effect [4], and Urban Moisture and Dry Islands (UMI and UDI) effect [5, 6]. The temperature differential may amplify climate change and heatwaves in metropolitan areas, thereby affecting the energy demand for buildings [7-10]. In contrast, rural areas, while still subject to global climate change, typically experience less thermal amplification, leading to different energy use patterns and adaptation challenges [11-13]. This urban-rural dichotomy necessitates the development of tailored strategies for climate resilience.

Situated along the southern Chinese coastline, Hong Kong is defined by a humid subtropical environment [14]. This city faces challenges in energy efficiency and sustainable building management, exacerbated by its persistently humid conditions, exceptionally high population density, and a vast, aging building stock [15, 16]. In response to the substantial share of total urban energy demand and carbon emissions attributed to the building stock, the government announced Hong Kong's Climate Action Plan 2050 for carbon neutrality, including strategies to improve the energy efficiency of buildings to reduce the energy demand [17]. . Among all the residential building types, Hong Kong's public rental housing (PRH) plays a crucial role as it accommodates approximately 2.09 million residents, accounting for about 28% of the total population in Hong Kong [18]. This highlights the significance of studying how

climate change influences the cooling energy demand of PRH.

As global climate shifts, sustained episodes of extreme thermal intensity across vast geographic areas have emerged as a critical point of concern. These prolonged heat events represent a growing threat to regional stability and public health [19]. The frequency and severity of heatwaves are increasing worldwide. In particular, extreme heatwave events were found to demonstrate more notable changes throughout the 1991–2020 interval, surpassing the trends observed in previous years [20]. The extreme warmth during heatwaves could significantly affect the energy consumption of buildings [19, 21, 22]. One of the major consequences is the significantly increasing air-conditioning (AC) load for space cooling [23]. The share of energy use attributed to air-conditioning in residential buildings rose from 23% in 2012 to 27% in 2022 [24]. In Hong Kong, the impacts on urban microclimate are further intensified due to amplified Urban Heat Island (UHI) phenomena within the distinctive high-density spatial configurations [25], characterized by high-rise buildings in urban areas, street canyons with high aspect ratios, limited green spaces, and extensive impervious surfaces [4]. The impact of UHI can contribute to a rise in building cooling energy demand. Recent studies revealed a substantial positive correlation between daytime UHI effect and building cooling load [26]. The synergetic effect of UHI and heatwaves can further amplify urban overheating and increase building cooling load [19, 27].

Climate conditions in urban and rural areas exhibit significant disparities. Urban areas often experience more severe heatwaves than rural areas [28], which further increases the building cooling load [21]. Apart from the impact of heatwaves, the urban-rural disparity in building cooling loads can also widen as the intensity of the Urban Heat Island (UHI) effect increases [21, 29]. Each 1°C increase in the UHI effect can raise cooling energy consumption by approximately 7.9% in summer and 16.1% in transitional seasons [30]. In Hong Kong, the UHI intensity in the urban center can be greater than 10°C [31]. This difference has significant implications for building energy consumption, where heatwaves are growing more frequent and severe due to climate change. Li et al. utilized Cooling Degree Hours (CDH) to quantify climate-driven cooling demand, comparing urban and suburban data across several regions,

including Hong Kong [32]. Their study found that cooling loads have been increasing annually, with urban cooling loads in Hong Kong approximately 12% higher than those in rural areas.

Numerous studies used building energy modeling (BEM) to evaluate the energy use of public rental housing in Hong Kong [14, 26, 30, 33-39]. Although these studies provide valuable insights into energy patterns and retrofits, they are constrained by the spatial and temporal resolution of weather datasets. BEM relies heavily on accurate weather inputs, including temperature, humidity, solar radiation, and wind speed, as essential inputs. The importance of weather data has been shown in BEM simulations in different climate regions [40-46]. Previous studies on public rental housing (PRH) in Hong Kong typically rely on either outdated local weather datasets—sourced from the Hong Kong Observatory or automatic weather stations located at sites such as the airport—or on Typical Meteorological Year (TMY) datasets as inputs for BEM [33, 34, 47-49]. TMY derived from historical data can also become outdated over time, making it inadequate for representing recent weather conditions [44, 50-52]. Moreover, TMY data do not represent the specific microclimatic conditions at the exact location of the PRH buildings, potentially affecting the estimation of cooling demand differences.

This reliance on generalized datasets is particularly problematic when predicting the cooling load in air conditioning systems, which comprises two main components: sensible cooling, driven by air temperature, and latent cooling, which accounts for the energy needed to remove moisture from the air [53, 54]. Maia-Silva et al. highlighted that rising temperatures are associated with increased humidity in climate change, and the combination of increased air temperature and humidity could significantly increase heat stress and electricity demand during extreme heat events [55]. Cao et al. proposed a novel index combining air temperature and relative humidity to examine how latent cooling demand responds to variations in temperature and humidity across China's diverse climate regions [56]. As a result, this index shows a strong relationship with the examined latent cooling load. Their findings also indicate that air temperature is not sufficient to characterize the climate sensitivity of cooling load [55]. Meanwhile, a study by Kheiri et al. revealed that different moisture levels can significantly

impact building energy consumption [57]. Aside from the UHI effect, the urban moisture island (UMI) effect is also crucial to building cooling load. The UMI effect has been found to increase latent cooling demand in summer in residential buildings in Hong Kong by up to 96% [6]. However, most BEM studies on PRH in Hong Kong only consider the total cooling load, without separately analyzing sensible and latent components. Multiple studies have analyzed both components to understand the impact of urban microclimate [19, 54, 58]. However, limited attention has been paid to how urban–rural climatic differences influence both sensible and latent cooling loads under extreme heatwave and how these responses vary spatially within a city.

The present study intends to address the following questions: (1) To what extent do urban–rural climate disparities influence the sensible and latent cooling loads of PRH in the subtropical high-density city Hong Kong? (2) How does the urban–rural contrast in cooling energy demand during EH and NS days vary by location, time of day, and floor level?

Numerical simulations driven by in-situ measured weather data are employed to investigate the impact of urban-rural weather differences on the cooling load of PRH buildings in Hong Kong. The remaining article is organized as follows: The methodology is illustrated in Section 2, including PRH site and building information, weather data generation, and BEM settings. Section 3 provides the results of climate characteristics and cooling load performance. The key findings and conclusions are discussed in Sections 4 and 5, respectively.

2. Methodology

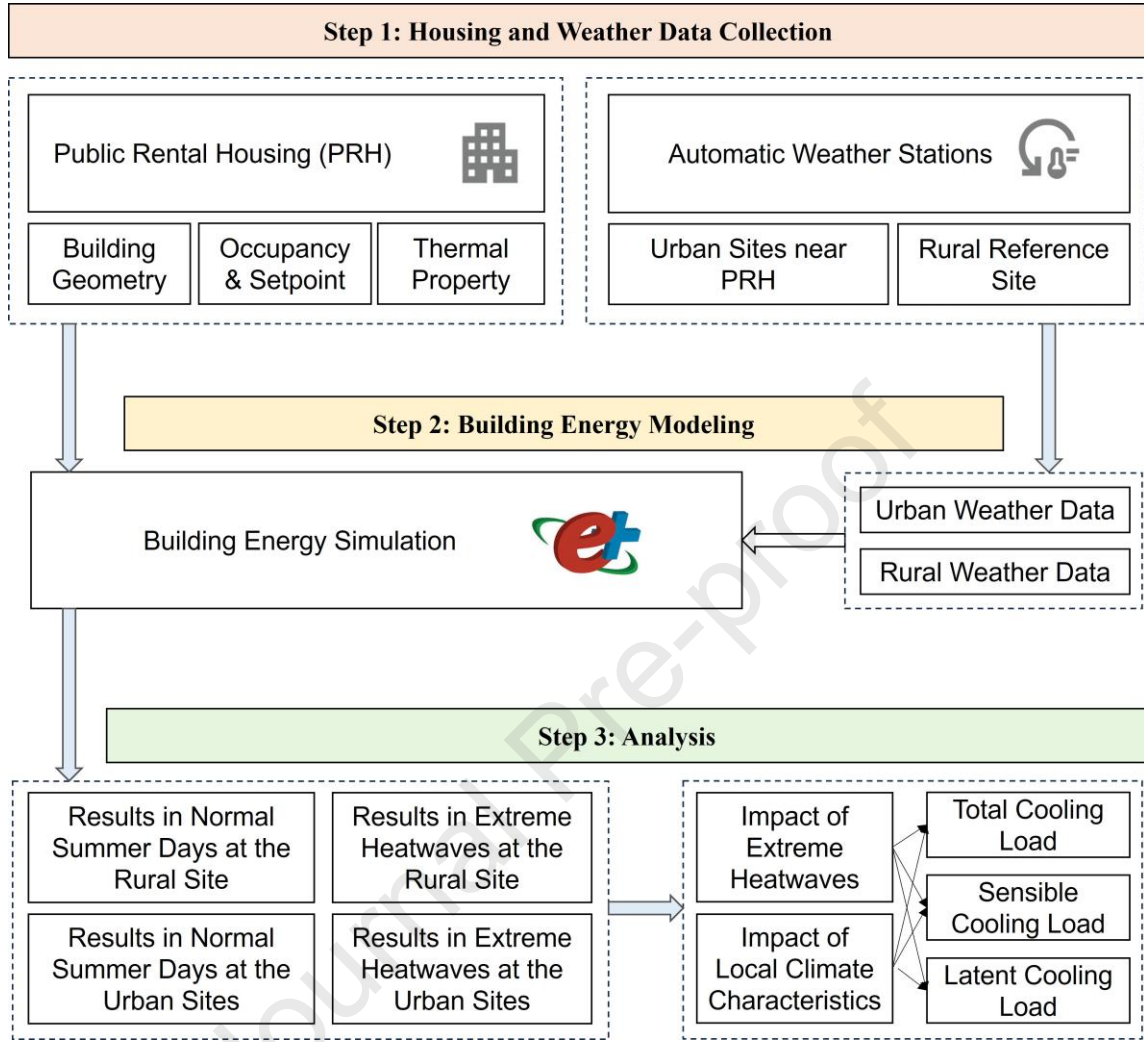


Figure 1 Research Framework

The present study involves three stages. First, measured weather data from weather stations in urban and rural sites were collected and converted into corresponding weather files for BEM. In the second stage, these weather files were used in EnergyPlus to model building energy consumption under different scenarios. Specifically, simulations were run for both normal summer days and extreme heatwave days at the rural reference site and urban sites (the definitions of normal summer days and extreme heatwave days will be given in Section 2.3). In the final stage, the simulated results of climate characteristics and cooling loads were compared to evaluate the impact of heatwaves on urban climate and building energy use.

2.1 Data Collection

2.1.1 Public rental housing

The present study focuses on PRH buildings built around the year 2000 across different areas in Hong Kong. Four typical PRH estates were selected as case studies (Figure 3), reflecting different urban microclimate scenarios with varying UHI intensities at the Tertiary Planning Unit scale, based on the classification in Ref [26]. Three are located in urban areas on the Kowloon Peninsula: (i) Hoi Fu Court in Mong Kok, Yau Tsim Mong District; (ii) Chung On Estate in Ma On Shan, Sha Tin District; (iii) Kwong Ming Court in Junk Bay, Sai Kung District; The other one is on an island but within a built-up town area, i.e., (iv) Nga Ning Court in Cheung Chau, Islands District. Table 1 shows the information about selected PRH estates [59]. All the selected buildings are of Harmony block type due to their high prevalence amongst newer PRH estates [37]. The typical plans of buildings are shown in Figure 2 [60].

Table 1

Information on selected PRHs

Name	Year of completion	No. of stories	No. of flats per story	Nearby weather station
Hoi Fu Court	2000	35	18	King's Park (KP)
Chung On Estate	1996	38	18	Sha Tin (ST)
Kwong Ming Court	1998	38	16	Junk Bay (JKB)
Nga Ning Court	2001	5	29	Cheung Chau (CCH)

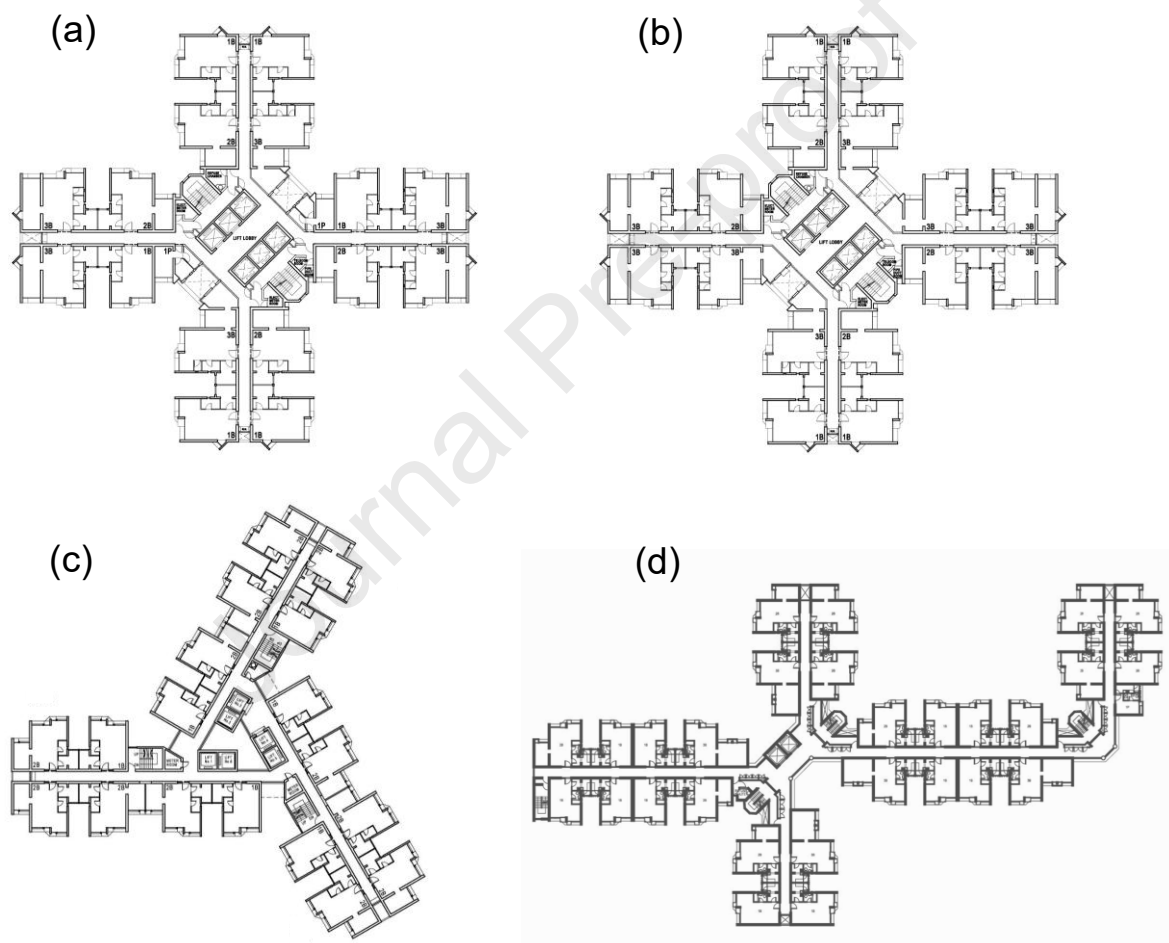


Figure 2 Typical floor plans of (a) Hoi Fu Court, (b) Kwong Ming Court, (c) Chung On Estate, and (d) Nga Ning Court. Plans are not drawn to the same scale.

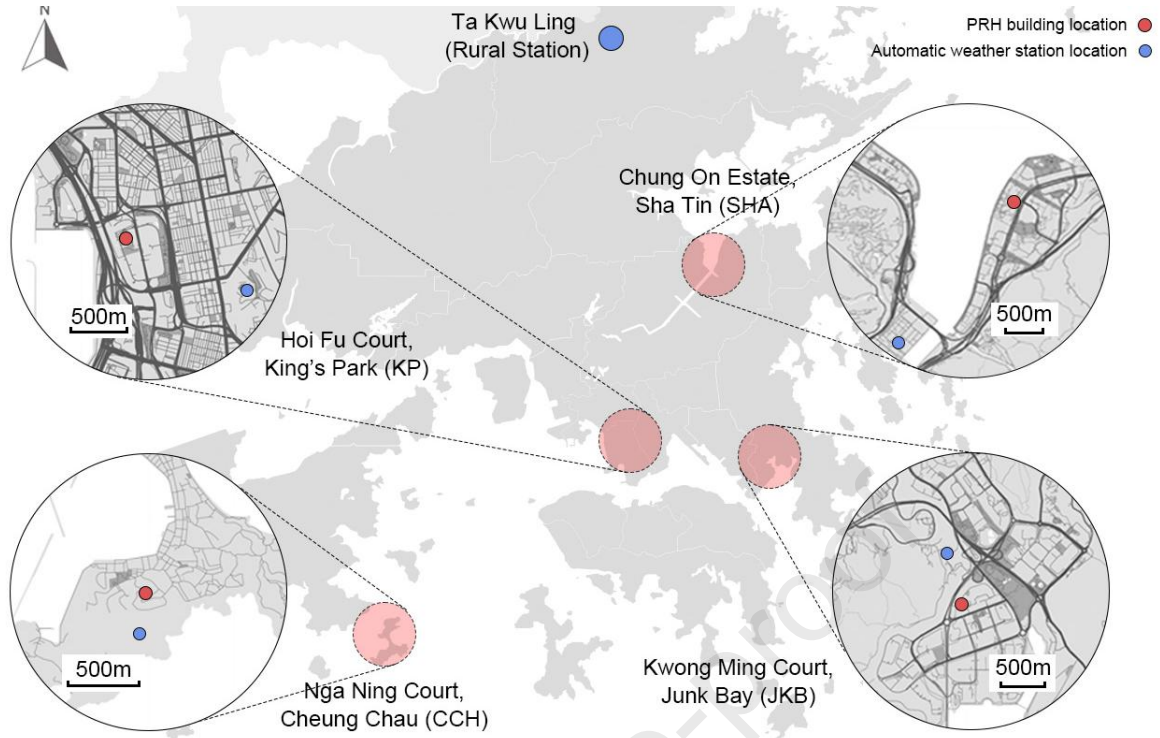


Figure 3 Locations of selected PRHs and automatic weather stations. The zoomed-in locations of each PRH site are not drawn to the same scale.

2.1.2 Weather data

Weather data from 2022 to 2024 were obtained from the Hong Kong Observatory, measured by the nearest automatic weather stations to the selected PRH estates, as the updated source of climate inputs to represent the accurate urban microclimate information for BEM. The distance between the weather stations and the selected PRH estates is less than 3 km (Figure 3). In the present study, Ta Kwu Ling, a typical rural site, was selected as a reference site to retrieve rural weather data in Hong Kong for urban-rural comparative analysis, consistent with early studies [61, 62].

The meteorological parameters include air temperature, humidity, mean sea level pressure, solar radiation, wind speed, wind direction, rainfall, etc. The information about the weather station is detailed in Table 2. Note that solar radiation data are only available at King's Park (KP) in the Hong Kong Observatory datasets. Global solar radiation, direct normal radiation, and diffuse solar radiation at KP were collected and applied to all sites.

Table 2

Information on the measurement of the local weather data [63]

Automatic weather stations	Corresponding PRH site	Location	Relevant meteorological parameters*
King's Park (KP)	Hoi Fu Court, Chung On Estate, Kwong Ming Court, Nga Ning Court, Rural Reference Site	22°18'43"N, 114°10'22"E	WS, WD, T, RH, P, R, SR
Sha Tin (SHA)	Chung On Estate	22°24'09"N, 114°12'36"E	WS, WD, T, RH, P, R
Tseung Kwan O (JKB)	Kwong Ming Court	22°18'57"N, 114°15'20"E	WS, WD, T, RH, R
Hong Kong Observatory (HKO)	Kwong Ming Court	22°18'07"N, 114°10'27"E	P
Cheung Chau (CCH)	Nga Ning Court	22°12'04"N, 114°01'36"E	WS, WD, T, RH, P, R
Ta Kwu Ling (TKL)	Rural Reference Site	22°31'43"N, 114°09'24"E	WS, WD, T, RH, P, R

* WS - Wind Speed; WD - Wind Direction; T - Temperature; RH - Relative Humidity; P - Mean Sea Level Pressure; R - Rainfall; SR - Solar Radiation

Weather data with all meteorological parameters was adopted to develop the annual EPW files as input for BEM from 2022 to 2024. Dew point temperature in EPW files was calculated based on dry bulb temperature, relative humidity, and atmospheric pressure. Since atmospheric pressure data for JKB is unavailable, the atmospheric pressure data from the Hong Kong Observatory weather station (HKO), the closest station containing atmospheric pressure data, was used for Kwong Ming Court.

2.2 Building energy modeling

EnergyPlus, a prominent open-source building energy simulation architecture, was employed in the present study. The study period for the 3 years is from June 1st to September 30th. The parameters of BEM for building geometry, thermal properties, HVAC system and

occupancy schedules were adopted from previous studies [14, 19, 60, 64-69]. The specifications of the energy model are further elucidated within the following subsections:

2.2.1 Building geometry and material settings

The information on building geometries, including physical parameters, building components, and material properties, is listed in Table 4. The floor height of all buildings was set to 2.7 m [65]. Total occupied floor area, air-conditioned area, and window-to-wall ratio were calculated from building geometries based on floor plans from the Hong Kong Housing Authority (HKHA) [60]. Table 3 also shows the building components and material properties applied to the PRH buildings from a typical model according to the characteristics of the original construction [66, 68]. The PRH buildings investigated in the present study were completed between 1996 and 2001 and adopted similar material properties and construction codes to minimize the influence of building-specific factors.

BEM costs a massive computational time with thousands of air-conditioned zones on all floors over a 35-storey building. Therefore, simplification has been widely adopted by incorporating typical floors in building energy models [14, 33]. To reduce the number of air-conditioned zones for efficient simulation while ensuring accuracy, three representative residential floors (bottom floor, middle floor, top floor) were modelled with complete room layouts for each PRH building. Note that the bottom floors took the actual second level of each PRH building, since the actual first level is used for public amenities.

The building energy model also includes surrounding buildings as shading elements. Ground surface temperature data used in EnergyPlus simulation were retrieved from the fifth-generation ECMWF atmospheric reanalysis (ERA5) to more accurately simulate the heat flux of the bottom floor [70]. Building geometries of each PRH building in BEM are presented in Table 3.

Table 3

Building geometries of selected PRH buildings.

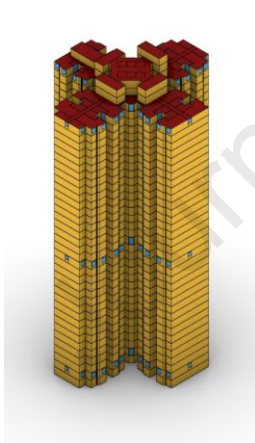
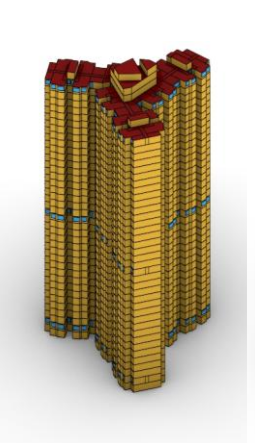
PRH Buildings	Hoi Fu Court	Kwong Ming Court	Chung On Estate	Nga Ning Court
Bird View				
Geometries of PRH Sites				
EnergyPlus model of PRH buildings				

Table 4

Building physical parameters, building components, and their properties in the BEM.

Building physical parameters	Hoi Fu Court	Kwong Ming Court	Chung On Estate	Nga Ning Court
Floor height (m ²)	2.7	2.7	2.7	2.7
Total occupied floor area (m ²)	43,552	46,490	47,355	8899
Air conditioned area (m ²)	24,490	27,612	26,573	5295
Building component	Material		U-value (W m ⁻² K ⁻¹)	
External Wall	13 mm gypsum plaster + 100 mm concrete + 13 mm cement/sand plaster		3.81	
Internal Partition	13 mm gypsum plaster + 100 mm concrete + 13 mm gypsum plaster		3.59	
Floor / Ceiling	5 mm vinyl tiles + 25 mm screed + 100 mm concrete		1.70	
Window	5 mm glass		5.82	
Door	6 mm plywood + air wall + 6mm plywood		3.75	
Material properties	Specific heat capacity (J kg ⁻¹ K ⁻¹)	Density (Kg m ⁻³)	Thermal Conductivity (W K ⁻¹ m ⁻¹)	
Concrete	653	2400	2.16	
Cement/sand plaster	840	1860	0.72	
Gypsum plaster	837	1120	0.38	
Wood	2093	800	0.16	
Glass	N/A	N/A	0.9	

2.2.2 Occupancy schedules

The cooling setpoint is set to 25°C for all the air-conditioned rooms in the PRH buildings, following Ref. [69]. It is also assumed that AC operates when rooms are occupied. During the AC operation period, all the windows are closed. The cooling schedules are based on an on-site survey conducted for the PRH buildings in Hong Kong [14], which provides the schedules

of all the units consisting of three types of rooms in the selected PRH buildings in this study: studio unit (a 1-person or 2-person suite), living room, and bedroom. Detailed occupancy schedules are displayed in Figure 4.

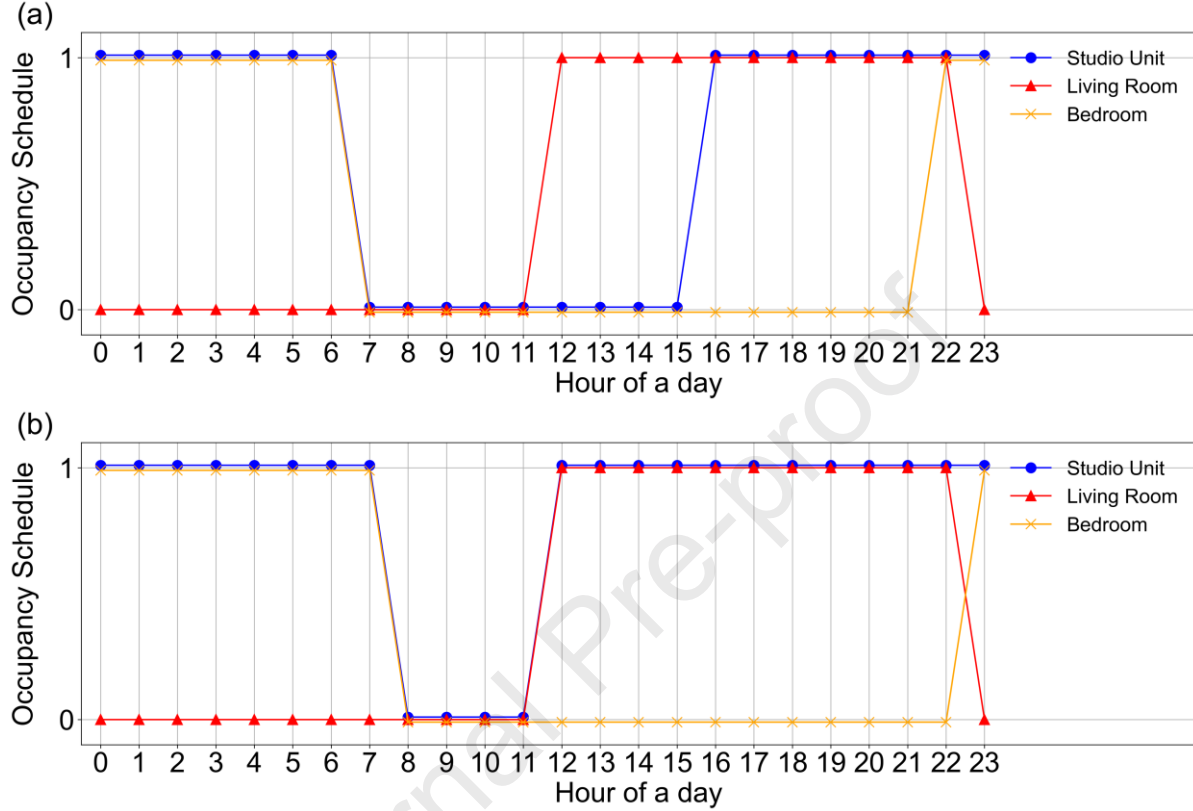


Figure 4 Occupancy schedule of Studio, living room, and bedroom (a) on weekdays and (b) weekends. “1” indicates full air-conditioning occupancy during this hour, while “0” indicates no occupancy

An Ideal Loads Air System [67] was adopted in EnergyPlus to evaluate the cooling demand of the PRH buildings. At each simulation timestep, EnergyPlus calculates the sensible and latent cooling loads required to maintain the indoor cooling setpoint under the prescribed weather conditions, building characteristics, and occupancy schedules. The total cooling load intensity (CL_{tot}) reported in this study is the sum of sensible cooling load intensity (CL_s) and latent cooling load intensity (CL_l).

2.2.3 Analysis methods

We defined two categories of weather days during the summer periods (June 1st to September 30th): extreme heatwave (EH) days and normal summer (NS) days (reference days).

A day with the maximum hourly temperature exceeding 35 °C [71] at the rural reference site is considered an extremely overheat day. An extreme heatwave event is defined as a sequence of at least three consecutive extremely overheat days. Days during such extreme heatwave events are defined as EH days. By comparison, an NS day must meet all the following three criteria: (1) this day is not a rainy day; (2) the diurnal temperature range (DTR) measured at the rural reference site must exceed the 50th percentile of DTR for the entire study period to avoid overcast days, as low DTR values typically indicate cloudy and overcast conditions [72]; (3) daily cumulative precipitation must be less than 0.1 mm to exclude rainy days [19]; The information about extreme heatwave events, and NS days are shown in Table 5.

Table 5

EH days, NS days, and the period of heatwave events in the study period

Year	Extreme heatwave events	No. of days in extreme heatwave events (EH days)	No. of NS days
2022	07-11 to 07-15; 07-21 to 07-29; 07-31 to 08-02; 09-12 to 09-15	21	26
2023	07-25 to 07-28	4	24
2024	08-03 to 08-09	7	22
Total	N.A.	32	72

3. Results

3.1 Weather conditions: air temperature and dew point temperature

In this section, the weather conditions were compared across four scenarios: NS days at urban sites, EH days at urban sites, NS days at the rural reference site, and EH days at the rural reference site. The meteorological parameters include air temperature, dew point temperature, and wind speed.

Figure 5 illustrates the air temperature (T_a) averaged for each hour across all days.

Significant differences are found across all the scenarios and locations. Daily T_a fluctuations are generally less pronounced at urban sites than at rural reference sites, with greater variation observed during EH days compared to NS days. For instance, the DTR in EH days and NS days at SHA are 6.95 °C and 5.34 °C, while the DTR at the rural reference site in EH days and NS days are 9.79 °C and 7.45 °C. As expected, T_a difference between EH days and NS days in the daytime is found to be more pronounced than that in the nighttime.

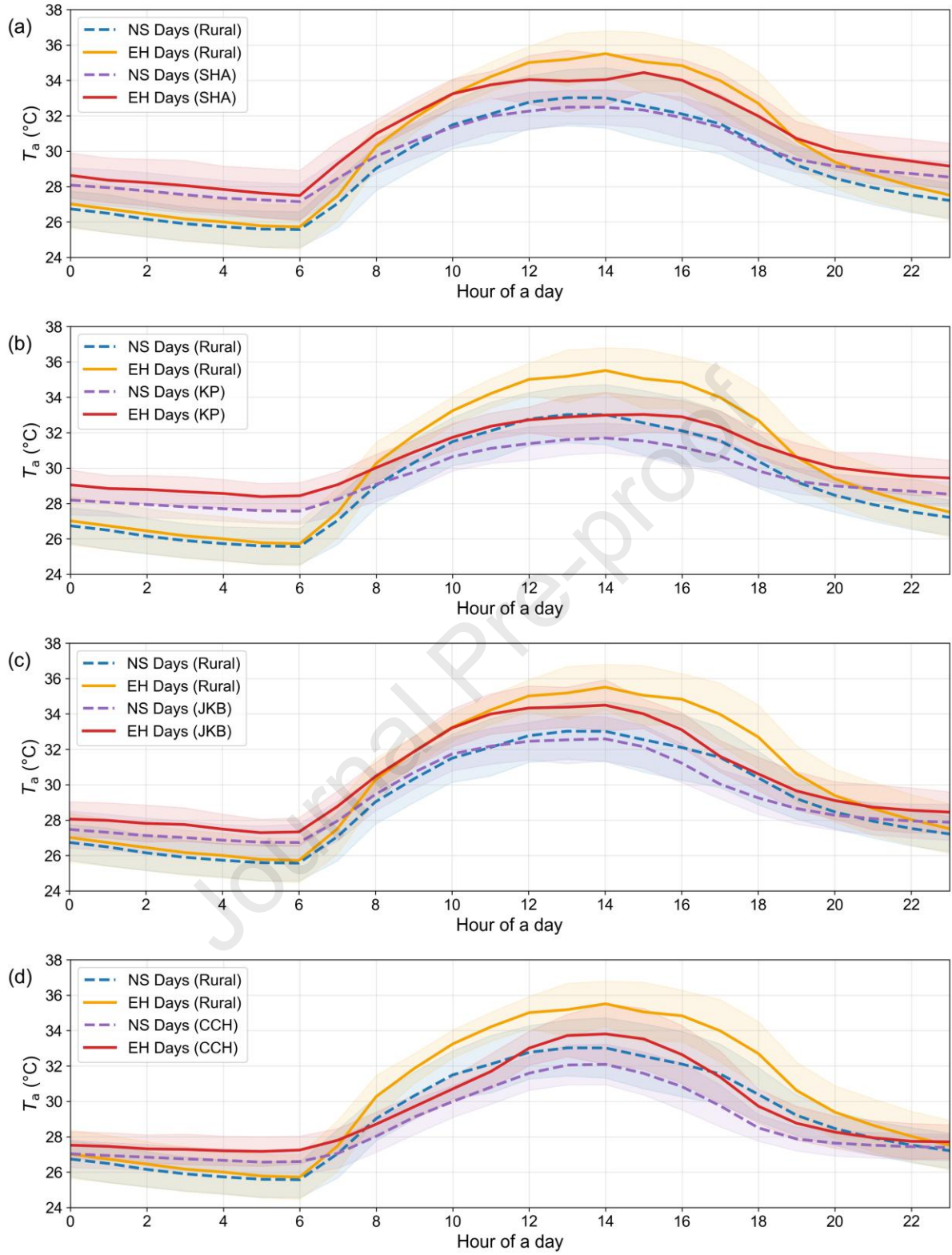


Figure 5 T_a averaged for each hour across all the days during the study period, measured by automatic weather stations in (a) SHA, (b) KP, (c) JKB, and (d) CCH. The solid lines denote the average values, while the shaded areas represent the standard deviations for the analyzed days over the study period. The rural reference data is added.

The peak T_a values (Figure 5) are similar across sites, ranging from 31.70 °C to 32.59 °C in NS days and from 33.03 °C to 34.50 °C in EH days. Overall, at night and in the early morning, T_a in urban areas is higher than in the rural reference site. While from the beginning of daytime, T_a at the rural site increases faster than in the urban sites and reaches higher peak values. This difference may be attributed to the shading provided by high-density buildings, which helps reduce heat gain. The magnitude of urban-rural air temperature differences varies across different locations. For example, the urban cool island (UCI) effect during daytime is found to be more pronounced in KP than in other sites in typical urban areas (SHA and JKB), in the averaged diurnal variation in both NS days and EH days. The UHI effect during nighttime is exacerbated by heatwaves, as the urban-rural T_a difference is higher in EH days than in NS days in all locations.

Figure 6 shows the daily variation of dew point temperature (T_{dew}), which displays a distinct pattern from T_a profiles. Overall, T_{dew} at urban sites is slightly higher than the rural reference site during EH days and NS days, except at KP. For SHA, JKB, and CCH, the magnitude of the UMI effect is greater in EH days than in NS days. The maximum daily urban-rural differences in the 3 sites are from 1.12 °C to 2.83 °C in EH days and from 0.62 °C to 1.92 °C in NS days, respectively. CCH shows the highest urban-rural difference of T_{dew} in both EH days and NS days.

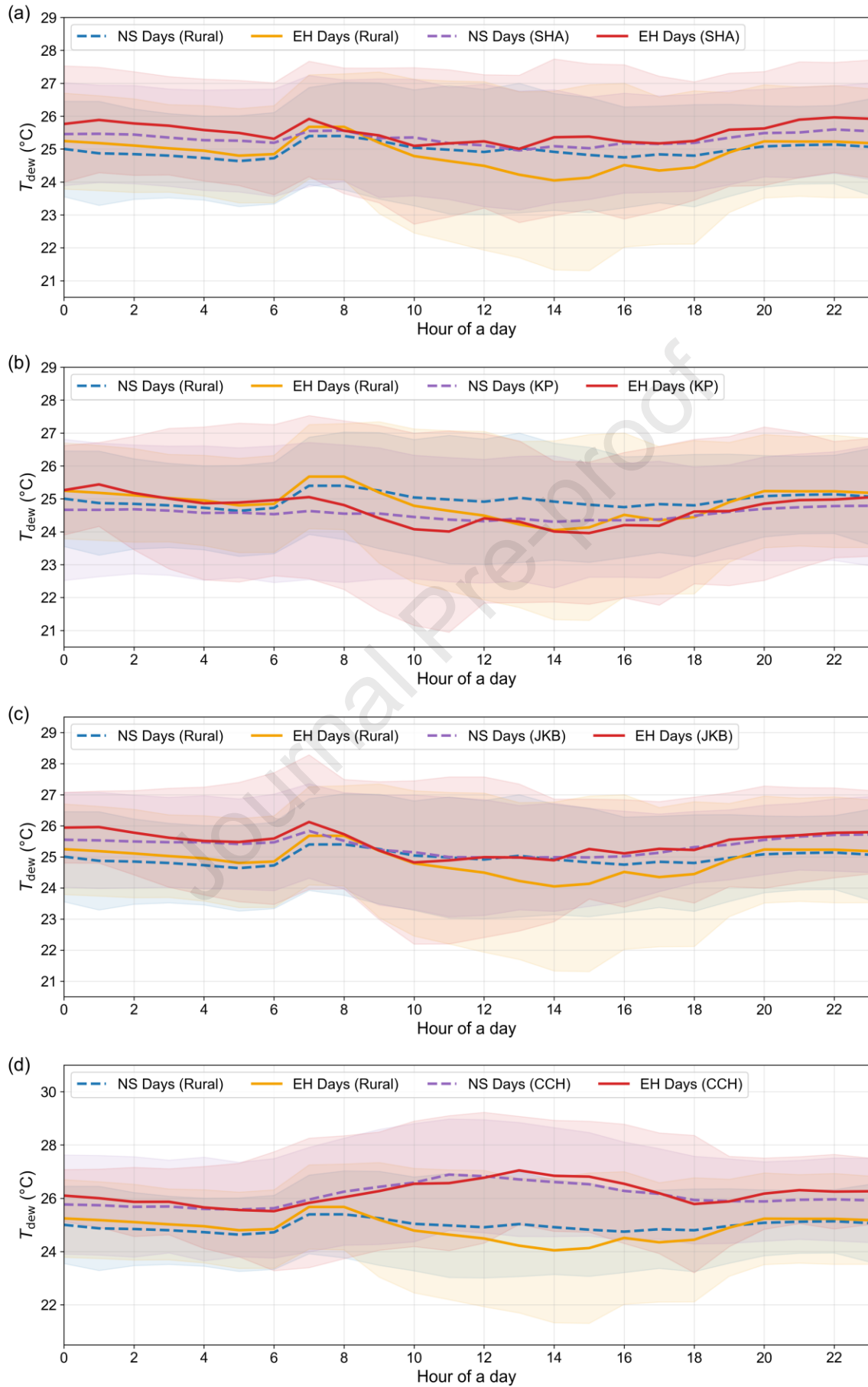


Figure 6 T_{dew} averaged for each hour across all the days during the study period measured by automatic weather stations in (a) SHA, (b) KP, (c) JKB, (d) CCH. The solid lines denote the average values, while the shaded areas represent the standard deviations for the analyzed days over the study period.

3.2 Diurnal profile of building cooling loads

Figure 7 shows the simulated hourly total cooling load intensity (CL_{tot}), and its two components: sensible cooling load intensity (CL_s), and latent cooling load intensity (CL_l), averaged for each hour across all days using urban and rural weather data for the four PRH cases. Urban weather data typically produces a higher CL_{tot} than the rural weather data during the midnight hours. For example, for KP cases, from 23:00 to 06:00, the urban-rural difference in accumulative CL_{tot} reaches up to 17.4% in EH days and 24.3% in NS days. In contrast, during the rest of the day (7:00 to 22:00), urban data tends to result in a lower CL_{tot} , with the accumulative CL_{tot} up to 7.4% in EH days and 6.5% NS days lower than the rural data. This urban-rural difference is mainly contributed by CL_s . In KP and CCH cases, daytime air temperatures at the rural reference site exceed those at the urban site due to reduced shading and stronger solar exposure, resulting in higher CL_s during daytime hours. Consequently, despite higher nighttime air temperatures in urban areas, the daily accumulated cooling load may be comparable to or even lower than that in the rural reference site. For CL_l , CCH case has a significantly higher value than the rural reference site from 7:00 to 22:00, while the urban-rural difference of CL_l in SHA, KP, and JKB is minimal. Notably, there is no cooling load between 8:00 and 11:00 due to the cooling schedule shown in Figure 6.

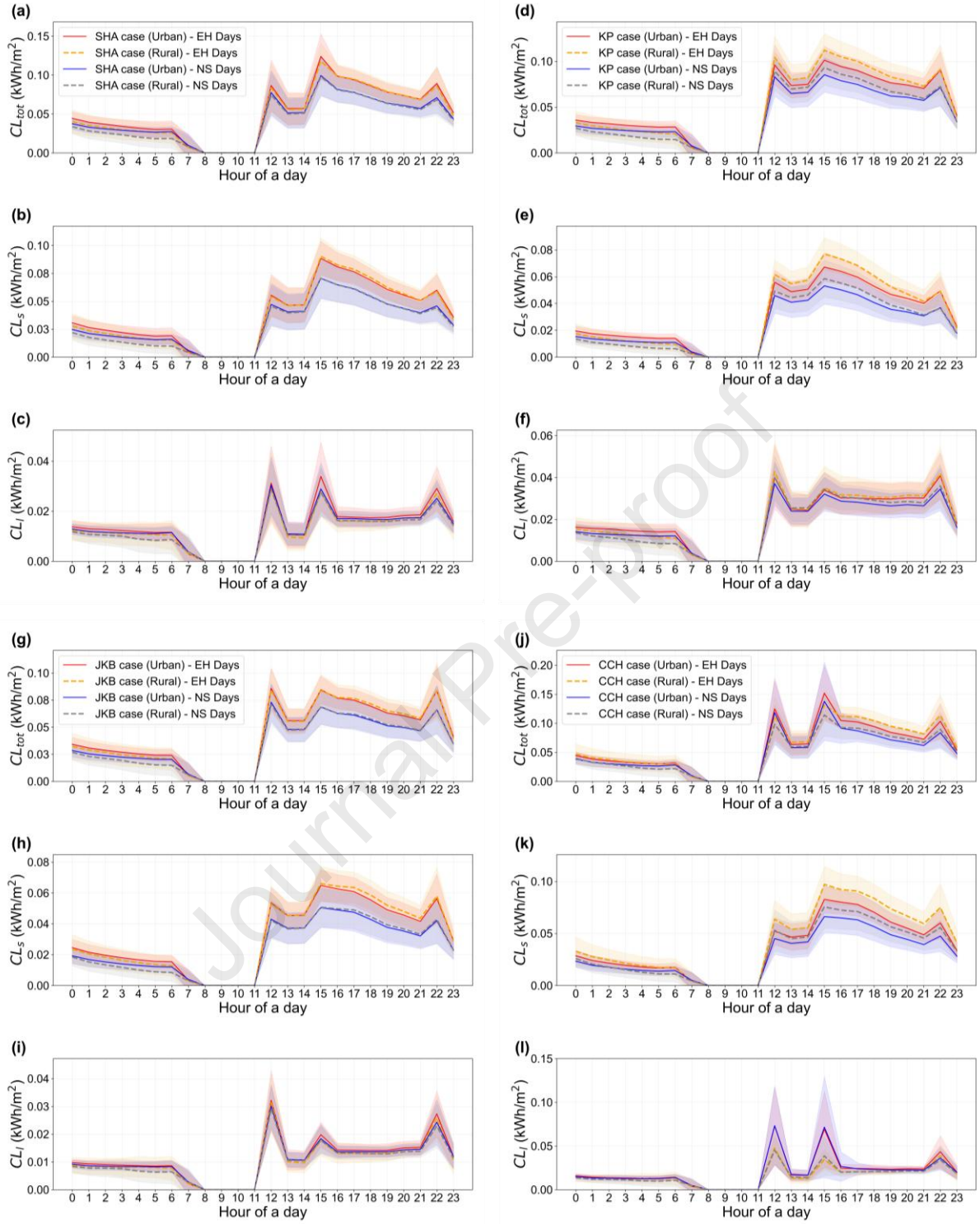


Figure 7 (a) CL_{tot} , (b) CL_s , (c) and CL_l using weather data from urban and rural reference sites averaged for each hour across all EH days and NS days of SHA, (d-f) the same for KP, (g-i) the same for JKB, and (j-l) the same for CCH PRH cases. The solid lines denote the average values, while the shaded areas represent the standard deviations calculated over the study period.

3.3 Daily mean accumulative building cooling load intensity

Figure 8 illustrates the daily mean accumulative CL_{tot} , CL_s , and CL_l of the bottom floor, middle floor, and top floor in 4 scenarios, averaged across the days in the study period among different PRH cases. As shown in Figure 8 (a), the three-floor-averaged CL_{tot} obtained from urban weather data in EH days is 4.0% and 1.3% higher than that using the rural weather data for SHA and JKB cases, respectively. This difference is more significant in NS days (6.4% and 3.1% higher for SHA and JKB cases, respectively). This is due to the significantly higher CL_{tot} in SHA and JKB than in the rural site from 23:00 to 6:00, as shown in Figure 7 (a-c) and (g-i). In contrast, the KP and the CCH cases exhibit an opposite urban-rural difference in EH days, with urban CL_{tot} 3.0% lower than rural CL_{tot} for KP case, and CL_{tot} 3.8% lower than rural CL_{tot} for CCH case. This is because of the lower urban CL_{tot} than the rural CL_{tot} from 7:00 to 22:00, as shown in Figure 7 (d-f) and (j-l). In NS days, the urban CL_{tot} is 1.4% lower for KP case, and 1.9% higher for CCH case. For all locations, CL_{tot} at the bottom and middle floors is generally close, while the top floor shows a tendency of higher cooling load demand. In urban sites, the daily mean accumulative CL_{tot} at the top floor can reach up to 16.8% higher compared to the bottom floor in EH days and 18.8% higher in NS days.

Figure 8 (b) and Figure 8 (c) show the daily mean accumulative CL_s and CL_l . In SHA, both the CL_s and CL_l align with the pattern of CL_{tot} , showing a higher value compared to that using weather data in the rural site. While in JKB, higher CL_{tot} and CL_l are observed compared to that using weather data in the rural site. For KP and CCH cases, when using rural weather data as BEM input, higher CL_s and CL_{tot} are observed for all floors compared to those using urban local weather data in EH days. However, when looking at the CL_l of CCH case, it is significantly higher in both EH days and NS days than that using rural weather data across all floors. This is because the higher T_{dew} is observed in the urban area despite the overall lower T_a , as shown in Figure 6 (d).

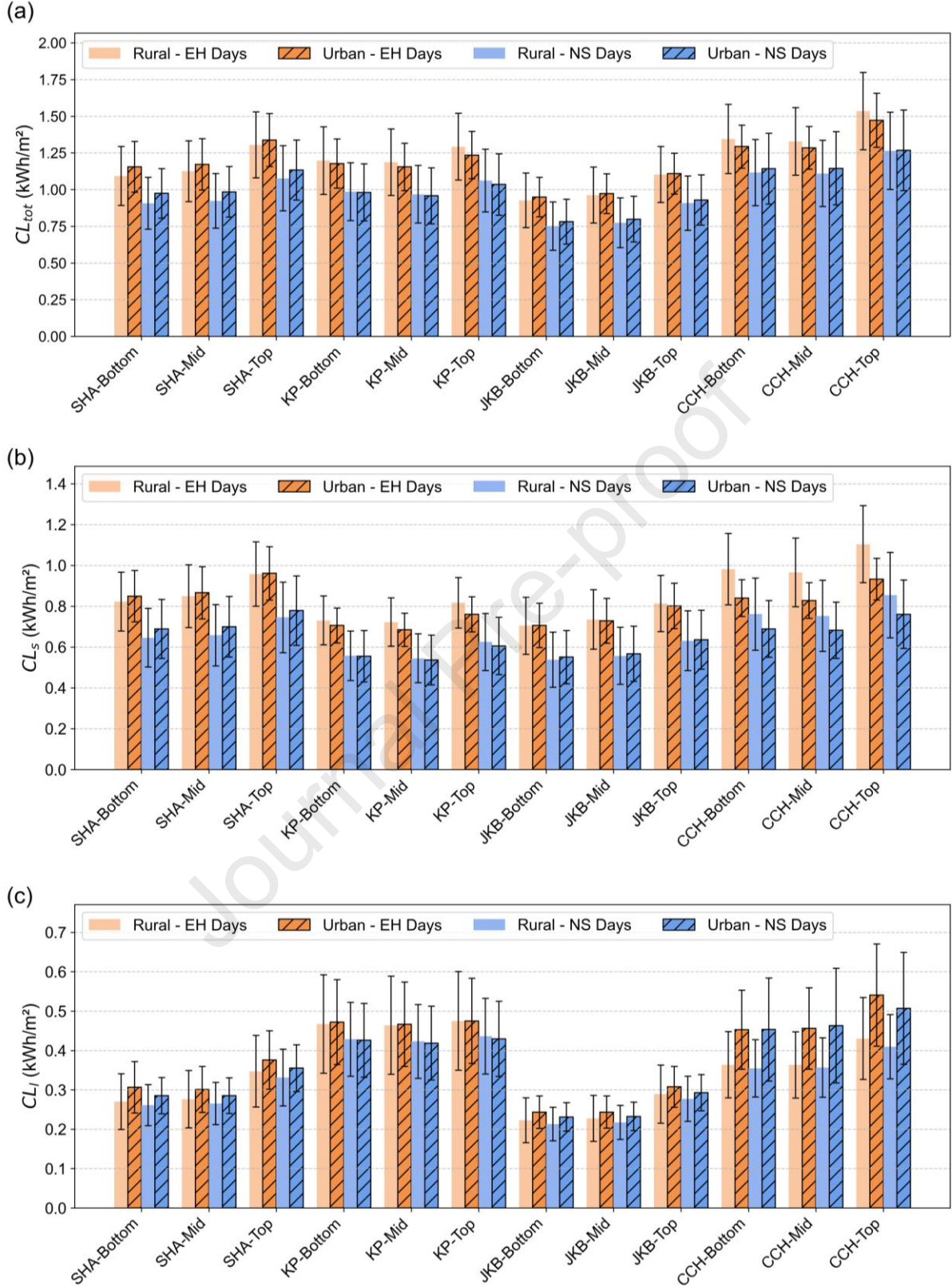


Figure 8 Daily mean accumulative (a) CL_{tot} , (b) CL_s , and (c) CL_l of different floors in 4 PRH building cases for all scenarios. The vertical error bars denote the corresponding standard deviation.

3.4 Daily peak building cooling load intensity

Precise quantification of maximum daily refrigeration requirements is fundamental for both HVAC system sizing and resilient metropolitan energy governance, especially when extreme heatwaves place unprecedented stress on the power grid [19]. Figure 9 shows boxplots of daily peak cooling load intensity in all locations under 4 scenarios. As shown in Figure 9 (a), the median value of daily peak CL_{tot} in SHA (6.5% in EH days and 3.2% in NS days) and CCH (9.3% in EH days and 22.6% in NS days) is higher than in the rural reference site, which is mainly contributed by CL_l shown in Figure 9 (c). In contrast, compared to the rural reference site, the median value of daily peak CL_{tot} in KP is 8.9% lower in EH days and 8.4% lower in NS days. CL_s dominates the urban-rural CL_{tot} disparities across different scenarios in SHA, KP, and JKB, as shown in Figure 9 (b).

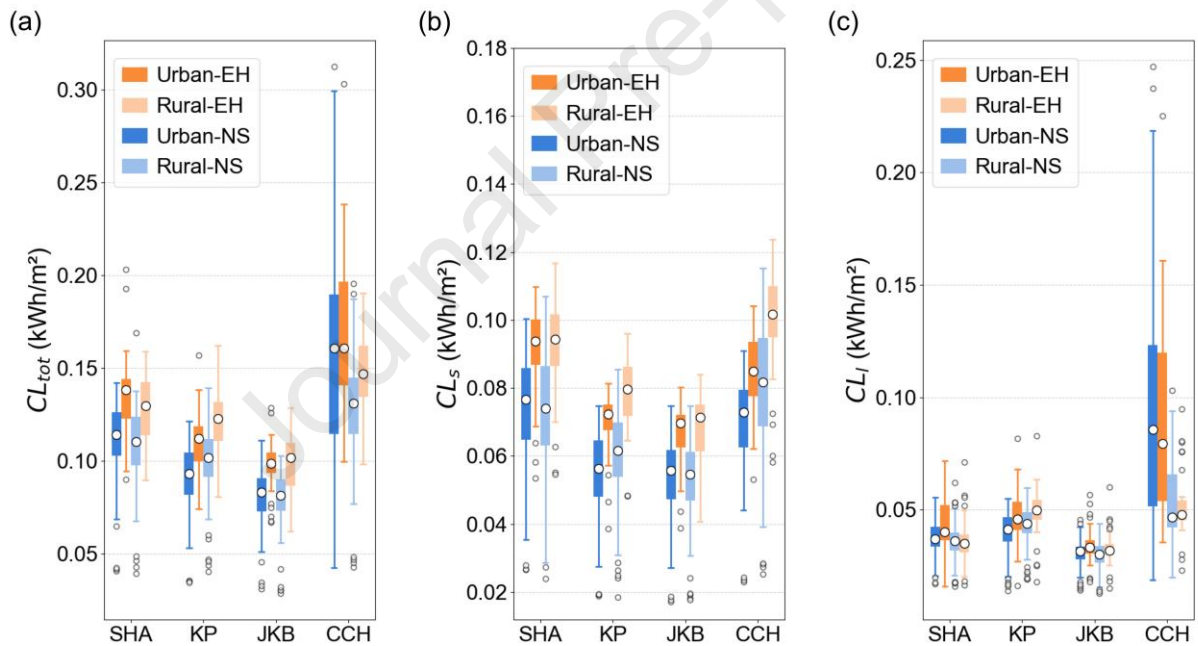


Figure 9 Boxplots of hourly peak (a) total, (b) sensible, and (c) latent cooling load intensity of four PRH building cases across different scenarios. Each box represents the interquartile range, spanning from the 25th percentile to the 75th percentile of the data. The circle within each box indicates the median (50th percentile), while the whiskers extend to the most extreme data points within 1.5 times the IQR from the lower and upper quartiles. Data points beyond this range are plotted individually as outliers.

3.5 Relationships of daily building cooling energy demand with T_a and T_{dew}

The daily cumulative CL_s and CL_l generally demonstrate a positive nonlinear correlation

with the daily mean T_a and T_{dew} . Linear and various degrees of polynomial regression were used to fit the model to illustrate the relationships. Figure 10 illustrates the relationship between daily mean T_a and daily mean accumulative CL_s in 4 PRH sites over the study period. The results in all 4 locations demonstrate a linear fit (CCH) or quasi-linear quadratic polynomial fit (SHA, KP, and JKB). The results for daily mean accumulative CL_s show that the model explains R^2 values ranging from 0.565 to 0.657, showing that the positive correlation between CL_s and T_a is robust. For every 1°C increase of T_a , the increase of CL_s ranges from 0.099 to 0.137 kWh/m^2 across different locations.

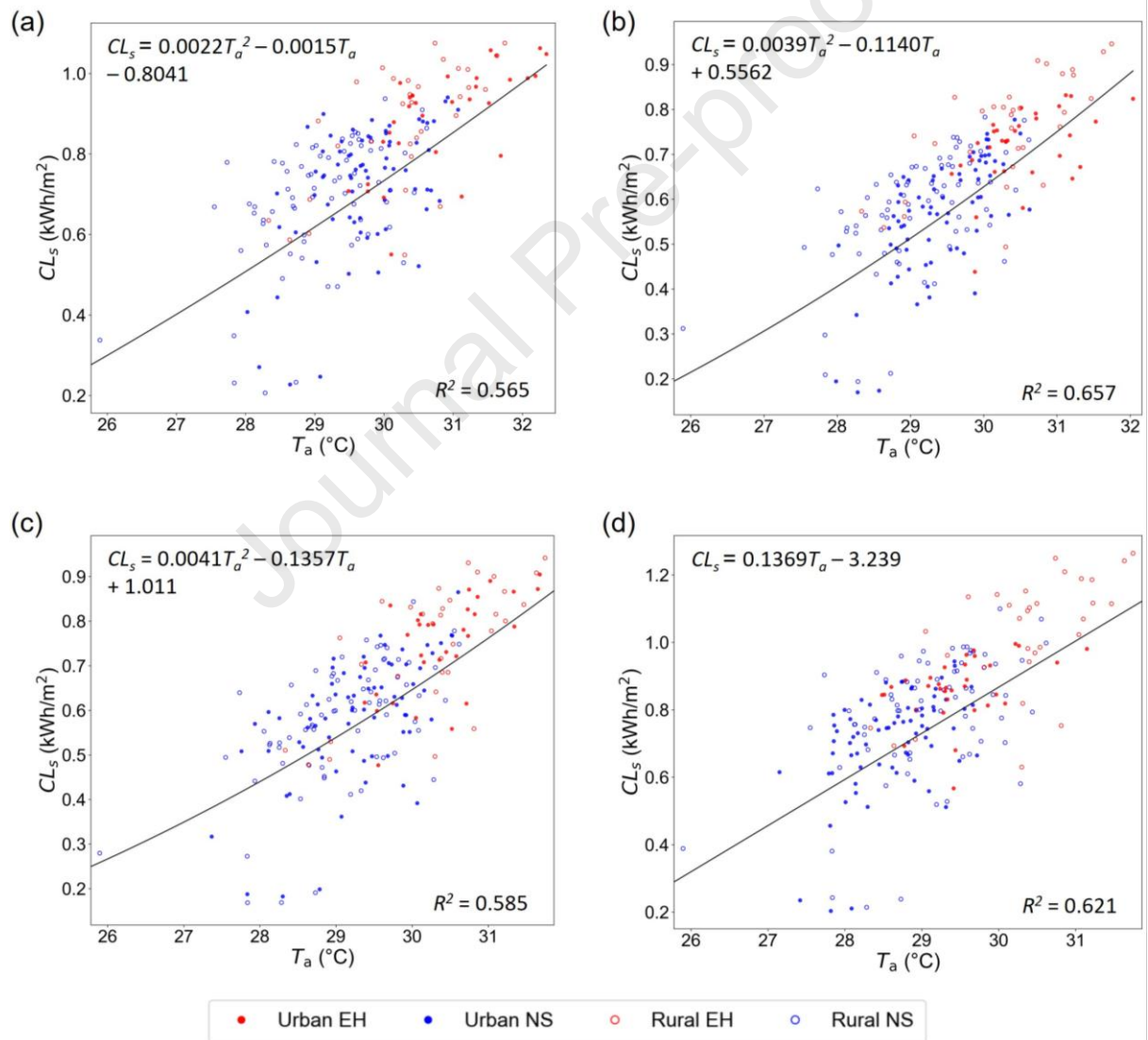


Figure 10 Relationships between daily mean T_a and daily mean accumulative sensible cooling demands of four PRH cases: (a) SHA, (b) KP, (c) JKB, and (d) CCH.

Figure 11 demonstrates the relationship between daily mean T_{dew} and daily mean accumulative CL_l . As a result, the overall R^2 ranges from 0.509 to 0.624 in different degrees of linear or polynomial models. The correlations between CL_l and T_{dew} are complicated in different locations and domains of T_{dew} . Overall, T_{dew} increases with CL_l from 20°C to 26°C. In SHA and KP, the increasing rate of CL_l fluctuates and could even fall to minus when T_{dew} is below 23°C. When T_{dew} is between 23°C and 26°C, every 1°C increase of T_{dew} can lead to a rise of CL_l from 0.029 to 0.075 kWh/m² across the 4 locations.

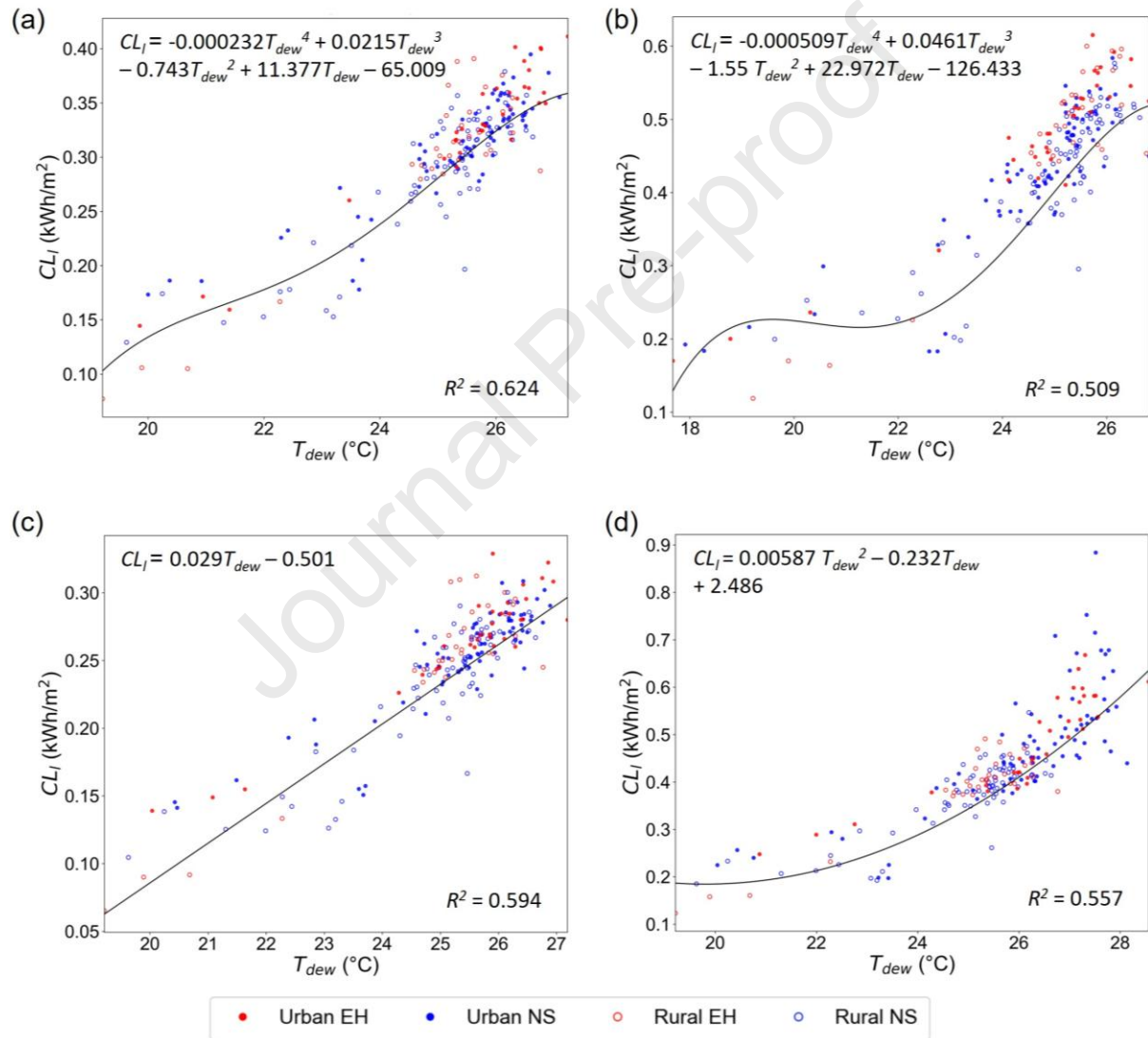


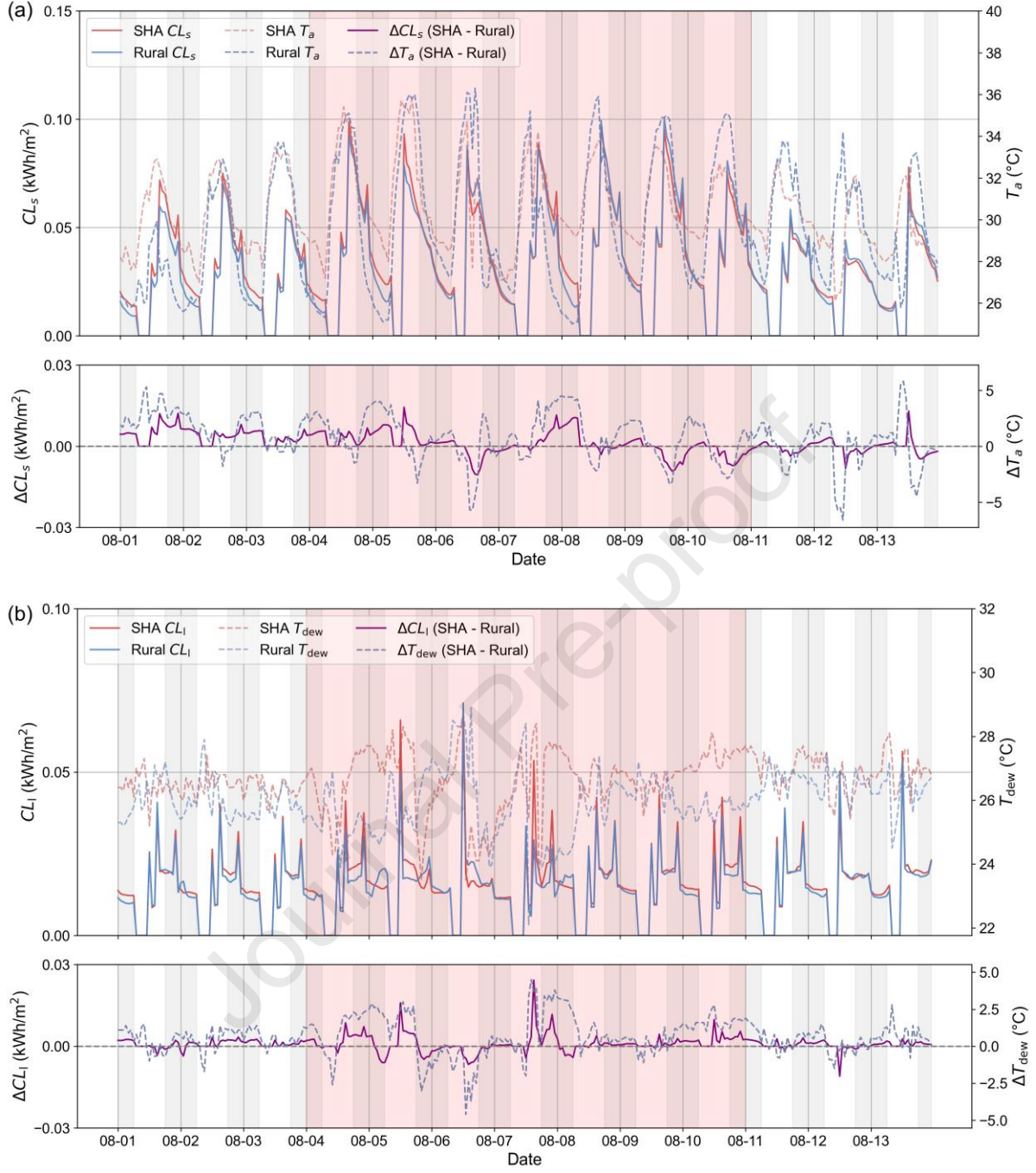
Figure 11 Relationships between daily mean T_{dew} and daily mean accumulative latent cooling demands of four PRH cases: (a) SHA, (b) KP, (c) JKB, and (d) CCH

3.6 Special EH event

An inspection analysis for a special EH event was conducted for an EH event at Chung On Estate, corresponding to SHA. Figure 12 shows the hourly profiles of CL_{tot} , CL_s , and CL_l simulated using urban and rural weather data as input to BEM, along with T_a and T_{dew} over 13 days from Aug 1st to Aug 13th, 2024. This period includes 3 pre-EH days, 7 EH days, and 3 post-EH days. In line with the observation in Figure 5a, T_a at nighttime is higher in SHA than in rural areas, exhibiting the UHI effect, while a UCI effect is observed during most daytime hours. After the mid-point of this EH event, T_a in the daytime is generally lower than in rural areas, indicating the urban cool island effect. T_{dew} , however, is generally higher during the entire selected EH event at SHA, showing a strong UMI effect.

Figure 12 (a) demonstrates the CL_s in this selected EH event, which is primarily influenced by T_a . Overall, the pattern of CL_s closely follows that of T_a . The result shows a higher cooling load in pre-EH days and a decline in the middle of this EH event. The variations of ΔT_a and ΔCL_s are generally aligned, except for several time lags (e.g., 12:00 on Aug 13th) and abrupt changes of cooling load due to the absent occupancy from 7:00 to 11:00 of PRH buildings (as explained in section 2.2.2), occurring after 11:00 every day. Regarding the CL_l (as shown in Figure 12 (b)), the result at SHA is generally higher than that at the rural site, which aligns with the T_{dew} variation. Similar to ΔCL_s , ΔCL_l experiences time lags and abrupt changes, due to the absence of occupancy from 7:00 to 11:00 (e.g., 12:00 on Aug 12th).

For the total cooling load, higher demand is observed in SHA than in the rural reference site during pre-EH days and the early stage of the EH event, as shown in Figure 12 (c). During the post-EH days, the daytime cooling load becomes generally higher at the rural site. At night, the cooling load in SHA remains consistently higher than that in rural areas during the first 2 days, while afterwards the difference between SHA and the rural site becomes minimal at night. This time lag could result from the effect of thermal inertia of PRH buildings and the prolonged heatwave.



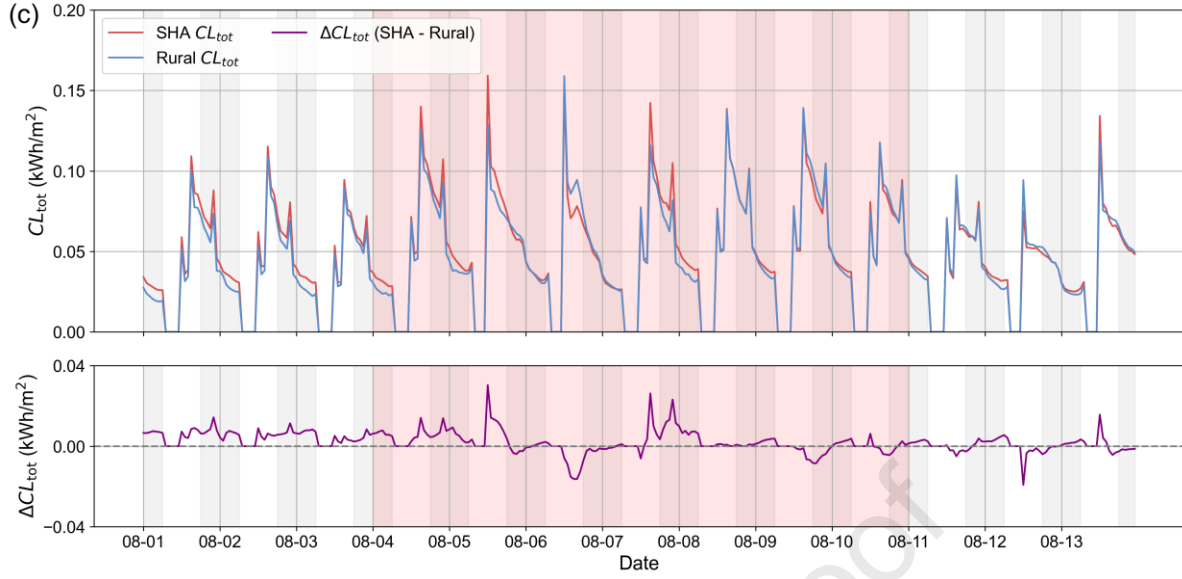


Figure 12 Hourly profiles and their urban-rural differences of (a) CL_s & T_a , (b) CL_l & T_{dew} , (c) total cooling load for Chung On Estate (SHA) from Aug 1st to Aug 13th, 2024. The red shaded periods denote the selected EH event days. The grey shaded periods denote nighttime hours from 18:00 to 06:00 the next day.

4. Discussion

4.1 Impact of heatwaves on building cooling load

The pronounced increase in CL_s during extreme heatwave (EH) periods is attributed to the rise in air temperature (T_a). Compared to normal summer (NS) days, the daily cumulative and peak cooling loads during extreme heatwave (EH) days are consistently higher. This pattern is evident in both urban and rural scenarios, though the magnitude of increase varies by site and weather conditions. The extended heatwaves and thermal inertia in building structures can influence passive thermal resilience [73], and have compounding effects where the daily cooling load varies differently from T_a . To mitigate the impact of heatwaves, technologies like radiative cooling are considered to have great cooling potentials during summer for its reduction in solar heat gain [74, 75]. In the climate conditions of Hong Kong, a previous study showed that a highly reflective material can generate a significant cooling effect on humid days [76].

Notably, while CL_s are primarily driven by outdoor T_a , CL_l appear more sensitive to the combination of internal moisture generation and elevated ambient humidity. CL_l 's increase in EH days (compared to NS days) is smaller than that of CL_s , yet it demonstrates a dynamic

response to higher T_{dew} . While air temperature remains the primary factor in temperature-driven cooling demand, humidity plays a secondary yet non-negligible role in influencing total energy demand. The strong relationship between T_{dew} and CL_l suggests that urban heat mitigation strategies should consider both air temperature and moisture-related effects. For example, nature-based solutions such as urban greening can reduce ambient temperatures through shading and evapotranspiration [74, 75], yet their effects on local humidity warrant evaluation, especially in humid subtropical regions where latent cooling accounts for much of total cooling demand. Integrated assessment of temperature and humidity responses is essential for developing effective adaptation strategies.

The top floors consistently experience higher CL_{tot} and CL_s compared to the middle and bottom floors, particularly under extreme heatwave (EH) conditions. They generally require more cooling energy to maintain the indoor T_a , primarily because of the greater heat gain through the exposed roof [77-79].

4.2 Urban-rural difference in building cooling load across locations

The urban-rural disparity in building cooling load reflects more than just a difference in T_a —it underscores the influence of building form, surface materials, ventilation characteristics, and microclimatic feedbacks [80, 81]. In the present study, the simulations revealed clear evidence of the UHI and UMI effects across the studied locations. In Sha Tin (SHA) and Junk Bay (JKB), urban weather data inputs yielded higher daily mean accumulative CL_{tot} than rural weather data inputs. The urban-rural gap is particularly evident at night, where retained urban heat limited cooling recovery, resulting in prolonged air-conditioning operation.

Notably, the site-specific variation in cooling load trends, particularly the reversal of humidity seen in Cheung Chau (CCH), suggests that urban-rural comparisons cannot rely on T_a alone. For CL_s , higher CL_s results are observed in Sha Tin (SHA) and Junk Bay (JKB) when compared to the rural area, while in KP and CCH, the CL_s results are higher in rural areas due to the lower T_a compared to SHA and JKB. The latent cooling load increases in CCH, possibly driven by local moisture accumulation or sea breeze-induced humidity.

4.3 Impact of occupancy on building cooling load

Occupancy behavior introduces a dynamic overlay to the patterns of cooling energy use [82, 83]. While temperature and humidity define the baseline load, it is the interaction with occupancy schedules and activity levels that sharpens the diurnal peaks observed in the simulated cooling load. The simulations incorporate dynamic schedules that reflect different occupancy levels during weekdays and weekends across unit types. The consistent rise in cooling load after 11:00 across all scenarios aligns with the appearance of occupancy. These findings underscore that occupancy schedules play a critical role in determining the actual cooling load profiles. Thus, they significantly amplify the impact of external climatic conditions. Dynamic variations in occupant behavior, appliance usage, and adaptive comfort responses can be incorporated. [84, 85].

4.4 Limitations and perspectives

Despite the robustness of this study in integrating measured weather data and detailed building energy modeling, several limitations should be acknowledged. First, the analysis focuses on four urban locations, representing typical conditions in Hong Kong. The variation in results across these sites indicates that a broader sample of PRH sites in urban areas is needed to enhance the generalizability of the conclusions. Note that expanding this work would require access to additional localized weather data for each new site. Second, this study used weather data in a 3-year period. Future work should consider using weather data over a longer period. In addition, the simulations adopted a fixed schedule and cooling setpoint (25°C) [69] to ensure consistent comparisons across scenarios. The present results underscore that occupancy schedules play a critical role in determining the actual cooling load profiles. Future studies can dynamically simulate variations in occupant behavior, appliance usage, and adaptive comfort responses.

5. Conclusion

This study provides a systematic assessment of how extreme heatwaves and urban microclimate conditions affect the building cooling energy performance of public rental housing (PRH) in Hong Kong. Four typical PRH sites were selected as urban cases; three are

located in urban areas on the Kowloon Peninsula, and one is on an island within a built-up town area. The analysis is based on building energy modeling using local measured weather data at urban sites and measured weather data at the reference rural site. The main findings can be summarized as follows:

- For the Extreme Heatwave (EH) events observed during the 2022–2024 study period, the urban–rural air temperature (T_a) difference is more pronounced during EH days than during Normal Summer (NS) days. At most urban sites, dew point temperature (T_{dew}) is higher than the reference site. This Urban Moisture Island (UMI) effect becomes more pronounced during the observed EH events.
- The urban-rural difference in daily accumulated total cooling load intensity (CL_{tot}) varies by urban site locations, ranging from 3.8% lower to 4.0% higher in urban sites than the rural reference sites in EH days. A diurnal pattern is observed: At night (23:00 to 06:00), accumulative total cooling load intensity is mostly higher than that from the reference rural site, reaching up to 17.4% higher in EH days and 24.3% higher in NS days. During the remainder of the day (07:00–22:00), the urban site generally results in a lower total cooling load intensity, up to 7.4% in EH days and 6.5% in NS days, lower than that from the reference rural site. The daily accumulated CL_{tot} shows a clear variation with floor level. Cooling load intensity at the bottom floor and the middle floor is generally similar. However, top floors require up to 16.8% (EH days) and 18.8% (NS days) more cooling load than bottom floors.
- During EH days, the median values of daily peak CL_{tot} across the four sites range from 8.9% lower to 9.3% higher than the rural reference. In NS days, this urban–rural contrast spans from 8.4% lower to 22.6% higher, reflecting stronger site-dependent dominance of either latent or sensible cooling load.
- CL_s show a moderately strong linear or quasi-linear correlation (R^2 ranges from 0.565 to 0.657) with T_a across different locations, with an increase from 0.099 to 0.137 kWh/m² per day for every 1°C increase in T_a . In contrast, CL_l exhibits a more complex correlation with T_{dew} across different locations with varying increasing rates.

- Occupancy schedules play a critical role in determining the actual cooling load profiles. The interaction between occupancy schedules and urban climate amplifies the impact of urban–rural climate differences on the overall cooling load.

The present study advances understanding of how extreme heatwaves and urban microclimate impact cooling energy demand in Hong Kong's public rental housing. These findings highlight the importance of considering the impact of urban microclimate on both sensible and latent cooling loads and provide new insights into the spatiotemporal variability of urban climate impacts on residential buildings in high-density subtropical cities. Furthermore, the pronounced spatial and temporal variations observed highlight the heterogeneous nature of urban climate impacts on buildings in high-density subtropical cities. These insights contribute to a more comprehensive understanding of urban climate–building energy interactions and provide a scientific basis for climate-responsive urban energy planning and adaptation strategies under intensifying heatwave conditions.

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Declaration of Competing Interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Highlights:

- Extreme heatwaves intensify Urban Heat and Moisture Island effects in Hong Kong.
- Nighttime urban cooling load is up to 17.4% higher than in rural areas in heatwaves.
- Urban cooling load in remaining hours is up to 7.4% lower than in rural areas.
- Latent cooling load results show complex, site-dependent humidity responses.
- Occupancy schedules can amplify the impact of urban–rural climate differences.

Declaration of Interest Statement

☒ The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

☐ The author is an Editorial Board Member/Editor-in-Chief/Associate Editor/Guest Editor for this journal and was not involved in the editorial review or the decision to publish this article.

☐ The authors declare the following financial interests/personal relationships which may be considered as potential competing interests:

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